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DESCRIPTION

ALLOYED STEEL POWDER WITH IMPROVED DEGREE OF SINTERING FOR METAL INJECTION MOLDING AND SINTERED BODY

TECHNICAL FIELD

[0001] The present invention relates to an alloyed steel powder for metal injection molding (MIM) which is effective to realize complex-shaped parts of very hard, highly corrosion resistant martensite stainless steel or tools of alloyed steel with good dimensional precision, and relates to a sintered body.

BACKGROUND ART

[0002] SKD11, SUS420, SUS440C and the like have conventionally been used as metal injection molding powders for obtaining very hard, highly corrosion resistant sintered bodies. These steels in which hardness is obtained by mainly use of Cr carbide exhibit an austenite phase in the sintering temperature range, and have a poor degree of sintering because the speed of elemental movement (diffusion) which promotes sintering is slower than in a ferrite phase. On the other hand, if the temperature is raised to the temperature at which a liquid phase appears in order to promote sintering, a large amount of liquid phase arises at once, carbides are formed as networks at the grain boundaries, and either the strength of the product is seriously diminished or it is deformed to the point that the shape of the product cannot be maintained. To avoid these, it is necessary to proceed with the sintering temperature controlled within an extremely narrow temperature range of ±5°C or in other words about 10°C. Because of this, it has been necessary to limit the usable

region of the sintering furnace, sacrificing productivity.

DISCLOSURE OF THE INVENTION

[0003] It is an object of the present invention to eliminate the aforementioned diminishment of product strength and difficulty of controlling sintering temperature which are problems of the aforementioned conventional sintering alloys, and to provide an alloyed steel powder for metal injection molding and a sintered body which contribute to enhancing product characteristics and improving productivity of the sintering furnace.

In order to solve the aforementioned problems, the present invention has the following constitution.

[0004] (1) An alloyed steel powder for metal injection molding with improved degree of sintering, consisting as mass percentages of 0.1 to 1.8% C, 0.3 to 1.2% Si, 0.1 to 0.5% Mn, 11.0 to 18.0% Cr, 2.0 to 5.0% Nb, and a remainder Fe and unavoidable impurities.

[0005] (2) An alloyed steel powder for metal injection molding with improved degree of sintering, consisting as mass percentages of 0.1 to 1.8% C, 0.3 to 1.2% Si, 0.1 to 0.5% Mn, 11.0 to 18.0% Cr, 5.0% or less of at least one of Mo, V and W, 2.0 to 5.0% Nb, and a remainder Fe and unavoidable impurities.

[0006] (3) An alloyed steel powder for metal injection molding with improved degree of sintering according to (2) above, wherein the at least one of Mo, V and W is 0.3 to 1.6%.

[0007] (4) An alloyed steel sintered body for metal injection molding with improved degree of sintering, consisting as mass percentages of 0.1 to 1.7% C, 0.3 to 1.2% Si, 0.1 to 0.5% Mn, 11.0 to 18.0% Cr, 2.0 to 5.0% Nb, and a remainder Fe and unavoidable impurities.

[0008] (5) An alloyed steel sintered body for metal injection molding with improved degree of sintering,

consisting as mass percentages of 0.1 to 1.7% C, 0.3 to 1.2% Si, 0.1 to 0.5% Mn, 11.0 to 18.0% Cr, 5.0% or less of at least one of Mo, V and W, 2.0 to 5.0% Nb, and a remainder Fe and unavoidable impurities.

[0009] (6) An alloyed steel sintered body for metal injection molding with improved degree of sintering according to (5) above, wherein the at least one of Mo, V and W is 0.3 to 1.6%.

[0010] The focus of the present invention is on producing a Nb carbide with low diffusion by adding Nb to a steel alloyed primarily with Cr carbide. Because this Nb carbide has a low diffusion speed it is unlikely to bulk by diffusion during sintering of the metal injection molded product, and the Cr carbide is also precipitated around the core of this Nb carbide.

[0011] Using the pinning effect of this Nb carbide it is possible to prevent from bulking and network formation of the carbide more effectively than when only the Cr carbide is present.

[0012] In the constitution of the present invention, C forms carbides and contributes hardness, resulting in a martensite structure. 0.1 to 1.8% is desirable as the amount range of C in the powder. The sintering temperature and sintered density vary according to the amount of C. Consequently, graphite is added appropriately during molding of the powder to adjust the amount of C in the sintered product to 0.1 to 1.7%. A sintered body with a high sintered density can be manufactured under easy temperature control. The lower limit of 0.1% in both powder and sintered body was set because that is the minimum amount necessary to produce the aforementioned Nb carbide and because it is the minimum amount at which the C would dissolve in the matrix to form martensite. The upper limits of 1.8% in the powder and 1.7% in the sintered body were set considering the amount of C

that is lost from the powder during sintering because at this level C contributes to hardness by forming a Cr carbide in the sintered body, but above 1.7% hardness is not further improved but on the contrary toughness (transverse rupture strength) is diminished.

[0013] Si improves deoxidation and hot water flow. If the amount is less than 0.3%, the oxygen amount rises and hot water flow is adversely affected, while if it is more than 1.2%, hardenability is adversely affected.

[0014] If Mn is less than 0.1%, hot water flow is adversely affected, while if it is over 0.5%, it combines with oxygen, increasing the amount of oxygen in the powder. Consequently, it is set in the range of 0.1 to 0.5%.

[0015] Cr improves hardenability and increases hardness by producing carbides. It also dissolves in the matrix including the carbides, thereby, it improves corrosion resistance. A range of 11.0 to 18.0% is desirable.

[0016] Mo, V and W produce carbides, and together with Nb have a pinning effect on the Cr carbides therefore they enhance the strength and hardness of the sintered body. If these are more than 5.0%, toughness will be diminished so 5.0% or less is desirable, and a range of 0.3 to 1.6% is more desirable from the standpoint of hardenability and cost-effectiveness. A noticeable improvement in hardness is difficult to achieve below 0.3%, while more than 1.6% is not cost-effective.

[0017] Nb controls diffusion of Cr carbides and improves hardenability by means of the pinning effect of low-diffusion Nb carbides. By adding 2.0 to 5.0% Nb, it is possible to improve the productivity of the sintering furnace because the sintering temperature needs only to be controlled within ±25°C rather than within ±5°C as it does conventionally. This effect isn't sufficient if the amount of Nb is less than 2.0%, while if it exceeds 5.0%, the amount of oxygen

increases and moldability is adversely affected.

BRIEF DESCRIPTION OF THE DRAWINGS

[0018] Figure 1 shows a pattern of sintering performed in an example of the present invention.

[0019] Figure 2 is a graph of the sintering characteristics of SKD11.

[0020] Figure 3 is a graph of the sintering characteristics of SUS420.

[0021] Figure 4 is a graph of the sintering characteristics of SUS440C.

[0022] Figure 5 is a graph of the sintering characteristics of Comparative Example 1.

[0023] Figure 6 is a graph of the sintering characteristics of Example 1 of the present invention.

[0024] Figure 7 is a graph of the sintering characteristics of Example 2 of the present invention.

[0025] Figure 8 is a graph of the sintering characteristics of Example 3 of the present invention.

[0026] Figure 9 is a graph of the sintering characteristics of Example 4 of the present invention.

BEST MODE FOR CARRYING OUT THE INVENTION

[0027] The samples shown in Table 1 below were prepared and their sintering characteristics tested.

Table 1

Steel type	Composition (%)										Dm (μm)	T/D (g/cm^3)
	C	Si	Mn	Cr	Mo	V	W	Nb	O	Fe		
SKD11	1.66	0.34	0.44	11.80	1.02	-	-	-	3300	Remainder	11.90	4.04
SUS420	0.27	0.85	0.33	13.09	0.59	-	-	-	3200	Remainder	10.01	4.30
SUS440C	0.96	0.91	0.18	17.12	0.05	0.07	-	-	2700	Remainder	9.72	4.21
Comp. Example 1	0.60	0.73	0.47	12.53	1.49	-	-	0.34	3900	Remainder	10.22	4.27
Example 1	1.03	0.92	0.22	17.01	-	-	-	3.01	4100	Remainder	9.92	4.17
Example 2	0.66	0.88	0.44	12.18	1.42	-	-	3.22	4200	Remainder	10.98	4.18
Example 3	0.96	0.87	0.21	17.12	0.41	0.17	0.08	2.99	3400	Remainder	9.86	4.08
Example 4	0.56	0.93	0.31	12.34	0.50	-	-	2.81	2500	Remainder	9.92	4.17
Comp. Example 2	0.65	0.89	0.45	12.15	1.46	-	-	7.33	13500	Remainder	10.34	4.20

[0028] The C amount of each sample was adjusted. Graphite powder was added with the aim of achieving C amounts after sintering of 1.30%, 1.50% and 1.70% for SKD11, 0.30%, 0.50%, 0.70% and 0.90% for SUS420, 1.30% for Example 1, 0.75%, 0.80%, 1.00% and 1.20% for SUS440C, 0.50%, 0.70% and 0.90% for Comparative Example 1 and Example 2, 1.30% for Example 3 and 0.90% for Example 4. A sintering test was not performed in the case of Comparative Example 2 because the amount of oxygen was too great at the powder stage.

[0029] The sintering test was performed as follows.

A suitable amount of graphite powder was added to each of the metal powders shown in Table 1, based on the target amount of C after sintering, 5.0 wt% of stearic acid (outer number) was added to the powder, and uniform kneading was performed with heating at 80°C.

[0030] The kneaded products were cooled to room temperature, and the solidified pellets were pulverized. The pulverized pellets were press molded at a molding pressure of 0.6 Ton/cm^2 (ϕ11.3 x 10t, N = 3).

[0031] Sintering was performed according to the pattern shown in Figure 1. In Figure 1, the sintering temperatures were the appropriate temperatures shown in Tables 2 through 5, such as 1370°C, 1390°C and 1410°C.

[0032] Tables 2 through 5 show the sintered density of each sample at different sintering temperatures and for different target amounts of carbon after sintering. The amounts of C, O and N in the sintered products of each sample are shown at the bottom of Tables 2 through 5, along with sintered hardness (Hv) in the case of Tables 4 and 5. The sintering characteristics shown in Tables 2 through 5 are also shown in graph form in Figures 2 through 9.

[0033] The structures were observed and the hardness of the sintered bodies was measured to determine the respective appropriate control ranges of sintering temperature. The

appropriate control range of sintering temperature was the sintering temperature range within which the sintered density remained nearly constant within a range of ±0.1 g/cm^3 as the sintering temperature rose on the sintering temperature-sintered density graph.

Table 2

Steel type		SKD11			Steel type		SUS420			
		Target C amount (%) after sintering					Target C amount (%) after sintering			
		1.30	1.50	1.70			0.30	0.50	0.70	0.90
Molded product Density		4.91	4.90	4.88	Molded product density		4.85	4.81	4.78	4.76
Sintering Tempera-ture(°C)	1220	-	-	6.84	Sintering Tempera-ture(°C)	1250	-	-	6.75	7.07
	1230	-	6.71	7.25		1270	-	-	6.82	7.47
	1240	6.81	7.20	7.61		1290	-	-	7.06	7.78
	1250	7.21	7.58	7.69		1310	6.82	-	7.38	7.91
	1260	7.68	7.70	7.69		1330	6.84	6.98	7.79	-
	1270	7.71	7.69	-		1350	6.86	7.27	7.85	-
	-	-	-	-		1370	6.92	7.70	-	-
	-	-	-	-		1390	7.41	7.69	-	-
	-	-	-	-		1410	7.70	-	-	-
C (%)		1.28	1.47	1.66	C (%)		0.33	0.57	0.79	0.99
O (ppm)		11	10	11	O (ppm)		17	40	27	41
N (ppm)		7	8	9	N (ppm)		3	4	1	3

Table 3

Steel type		SUS440C			
		Target C amount (%) after sintering			
		0.75	0.80	1.00	1.20
Molded product density		5.01	5.00	4.96	4.94
Sintering tempera-ture(°C)	1230	-	-	6.72	6.70
	1240	6.88	6.91	6.88	6.93
	1250	6.93	6.94	7.00	7.10
	1260	6.97	7.00	7.19	7.52
	1270	7.03	7.12	7.61	7.63
	1280	7.14	7.26	7.64	-
	1290	7.24	7.41	7.63	-
	1300	7.36	7.56	-	-
	-	-	-	-	-
C (%)		0.84	0.86	1.04	1.24
O (ppm)		130	60	42	34
N (ppm)		7	7	5	6

Steel type		Comparative Example 1		
		Target C amount (%) after sintering		
		0.50	0.70	0.90
Molded product density		4.68	4.69	4.69
Sintering tempera-ture(°C)	1270	5.44	6.23	7.38
	1290	5.71	6.92	7.77
	1310	6.50	7.75	7.77
	1330	7.31	7.76	-
	1350	7.77	-	-
	1370	7.77	-	-
	-	-	-	-
	-	-	-	-
	-	-	-	-
C (%)		0.54	0.76	0.96
O (ppm)		21	14	20
N (ppm)		3	2	13

Table 4

Steel type		Example 1	Steel type		Example 2		
		Target C amount (%) after sintering			Target C amount (%) after sintering		
		1.30			0.50	0.70	0.90
Molded product density		4.41	Molded product density		4.56	4.55	4.56
Sintering tempera-ture(°C)	1240	6.34	Sintering tempera-ture(°C)	1290	5.88	6.12	6.44
	1250	7.10		1310	6.79	6.98	7.27
	1260	7.68		1330	7.76	7.76	7.76
	1270	7.69		1350	7.76	7.75	7.75
	1280	7.70		1370	7.77	7.76	7.77
	1290	7.70		-	-	-	-
	1300	7.69		-	-	-	-
	1310	7.70		-	-	-	-
	-	-		-	-	-	-
C (%)		1.25	C (%)		0.52	0.73	0.94
O (ppm)		11	O (ppm)		26	22	32
N (ppm)		7	N (ppm)		10	8	7
Sintered hardness (Hv)		700	Sintered hardness (Hv)		600	640	310

Table 5

Steel type		Example 3	Steel type		Example 4
		Target C amount (%) after sintering			Target C amount (%) after sintering
		1.30			0.90
Molded product density		4.85	Molded product density		4.85
Sintering temperature (°C)	1230	-	Sintering temperature (°C)	1300	6.84
	1240	6.37		1310	7.25
	1250	7.14		1320	7.58
	1260	7.71		1330	7.83
	1270	7.72		1340	7.83
	1280	7.72		1350	7.83
	1290	7.72		1360	7.79
	1300	7.71		1370	7.77
	1310	7.72		1380	7.75
C (%)		1.35	C (%)		0.94
O (ppm)		46	O (ppm)		11
N (ppm)		28	N (ppm)		9
Sintered hardness (Hv)		749	Sintered hardness (Hv)		680

[0034] As discussed above, in the alloyed steel powder for metal injection molding of the present invention containing Nb, the appropriate sintering temperature control range is greater than in the case of SKD11, SUS420 and SUS440C. That is, while the appropriate sintering temperature control range is about 10°C in the case of SKD11, SUS420 and SUS440C, in the present invention it is broadened to about 50°C, facilitating sintering temperature control and improving productivity. The sensitivity to C value after sintering is also weaker, and almost the same sintering characteristics (temperature vs. density) are obtained with C values of 0.5 to 0.9%.